

Modelling autocatalytic behaviour of a food model system—Sucrose thermal degradation at high concentrations

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Abstract

Sucrose thermal degradation is an important reaction in the food industry. When in concentrated and neutral solutions, pure sucrose presents a lag phase in the reaction. This work aimed at: (i) modelling sucrose thermal degradation autocatalytic behaviour and (ii) studying the concentration and temperature effects on kinetic parameters. Isothermal experiments were conducted at temperatures ranging from 100 to 180 °C, using solutions with varying water content (3.58–30.03 % w/w). The logistic and Gompertz sigmoidal equations were modified and reparameterised, in order to describe degradation behaviour with kinetic parameters with physical meaning (maximum reaction rate, k_{\max} , and lag time, λ). In both models these parameters presented an Arrhenius type dependence on temperature. Following a mixed model effect methodology, the concentration dependence was observed on the Arrhenius parameters. This concentration effect was included in the proposed kinetic models, which were able to successfully describe experimental data.

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Keywords: Sucrose thermal degradation; Concentrated solutions; Autocatalytic reactions; Arrhenius and mixed model effects

1. Introduction

Sucrose thermal degradation is an important reaction in the food industry, since it is responsible for either important characteristics of the final food products or can influence the yield of obtainable white sugar in sugar manufacture. This degradation may occur by two different major reaction pathways: the Maillard reaction, which takes place in the presence of amino acids, and caramelisation, that occurs when sucrose is heated at high temperatures (BeMiller & Whistler, 1996). The Maillard reaction kinetics has been widely studied in the food science field (Baisier & Labuza, 1992; Buera, Chirifie, Resnik, & Wetzler, 1987; Imming, Buczys, Lehnberger, & Bliesener, 1996; van Boekel, 2001). Caramelisation, on the other hand, is considered to follow a simpler reaction pathway

and consequently fewer studies have been dedicated to its kinetics.

Caramelisation reaction is influenced by pH, impurities (salts) and sucrose concentration of the solution, and several authors approached these aspects (Clarke, Edye, & Eggleston, 1997; Eggleston & Vercellotti, 2000; Lowary & Richards, 1988; Mauch, 1971; Richards, 1986; Vukov, 1965). Most of those works are in a range of low sucrose concentration (<70% (w/w)), relatively low processing temperatures (<85 °C), presence of impurities and/or acidic or alkaline media (Mauch, 1971). A first-order model is often used to describe the heat degradation of sucrose under such conditions (Buera et al., 1987; Vukov, 1965). There is little information on the kinetics of sucrose thermal degradation at high concentrations. Schoebel, Tannenbaum, and Labuza (1969) studied sucrose degradation under these conditions. Still, this research was related to acidic saturated solutions and a first-order reaction was observed.

However, in some cases, like specific confectionery products (Davies & Labuza, 1997) or sugar boiling during white

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Nomenclature

a, b, c	mathematical parameters in the logistic and Gompertz equations	λ_{ref}	lag time at reference temperature (min)
C_1 to C_7	parameters of the global logistic and Gompertz models	MSE	mean square error
C	sucrose concentration (w/w (%))	p	kinetic parameter
C_0	initial sucrose concentration (w/w (%))	p_{ref}	kinetic parameter at finite reference temperature
e	Napier's constant	P	probability
E_a	activation energy (J mol^{-1})	R	universal gas constant ($8.314 \text{ J mol}^{-1} \text{ K}^{-1}$)
$E_{ak_{\text{max}}}$	activation energy for the k_{max} parameter (J mol^{-1})	R^2	coefficient of determination
$E_{a\lambda}$	activation energy for the λ parameter (J mol^{-1})	SE	standard error
k_{max}	maximum reaction rate (min^{-1})	SHW	standardised half with (%)
k_{maxref}	maximum reaction rate at reference temperature (min^{-1})	t	time (min)
λ	lag time (min)	T	temperature ($^{\circ}\text{C}$ or K)
		T_{ref}	reference temperature ($^{\circ}\text{C}$ or K)
		W	water content (w/w (%))
		x	independent variable
		y	dependent variable

sugar production (Richards, 1986), high concentrated sucrose solutions are heated at high temperatures, neutral pH and a lag phase on sucrose degradation occurs (Clarke et al., 1997; Eggleston, Trask-Morrel, & Vercellotti, 1996; Lowary & Richards, 1988; Richards, 1986). Eggleston et al. (1996) modelled such behaviour assuming a pseudo-first-order reaction for concentrated sucrose thermal degradation in the presence of different salts. A lag phase was also observed by Eggleston (2002) when studying cane juice stored at factory room temperature, where the sucrose degradation was due to the combined action of microbial, enzymatic and chemical reaction (acidic degradation). Haghghat-Khajavi, Kimura, Oomori, Matsuno, and Adachi (2005) found this type of behaviour in thermal degradation of sucrose in subcritical water (high pressure and high temperature conditions). An induction period was also observed in non-enzymatic browning of freeze dried model systems containing sucrose (Karel & Labuza, 1968; Labuza, Tannenbaum, & Karel, 1970).

The lag phase and consequent sinusoidal behaviour observed in pure, high concentrated and neutral solutions treated at high temperatures, suggests an autocatalytic type reaction. This autocatalytic nature is probably due to two main factors: (i) formation of weak acids during the first step of sucrose hydrolysis, that decreases solutions' pH and thus accelerates the reaction (Kroh, 1994; Lowary & Richards, 1988; Poncini, 1980) and (ii) molecular mobility. In the last decade, scientists started to realise the importance of molecular mobility, influenced by temperature and amount of water molecules in the system, in typical food reactions (Bell & Labuza, 1994; Karel, 1993; Kouassi & Roos, 2001; Slade & Levine, 1991). In sucrose hydrolysis, water can act as a solvent or reactant (Labuza et al., 1970). In concentrated solutions, there is a decreased molecular mobility in the system as well as a deficit in the available water molecules for the reaction to occur, which may explain the existence of a lag phase. Further-

more, studies on sucrose crystals indicate that sucrose degradation products depress the melting point, leading to a type of autocatalysis reaction by the increased molecular mobility (Poncini, 1981). In the amorphous state, the increase of molecular mobility during the reaction may also be explained by lower molecular weights of the degradation products (i.e. fructose and glucose) when compared with sucrose.

This work aims at modelling the reaction of sucrose thermal degradation at concentrated solutions, neutral pH and absence of impurities, where a lag phase is evident. To achieve that, experiments were carried out with concentrated sucrose solutions of 70–97% (w/w), treated at temperatures ranging from 100 to 180 $^{\circ}\text{C}$ for different times. The kinetic behaviour was mathematically described using the logistic and Gompertz equations, and the temperature and concentration dependence of the kinetic parameters was investigated.

2. Theoretical considerations

2.1. Modelling autocatalytic behaviour

An entire autocatalytic reaction, with lag and exponential phases, presents a sinusoidal shape resembling the microbial growth/inactivation behaviour. The logistic (Gibson, Bratchel, & Roberts, 1987; Neter, Knuter, Nachtsheim, & Wasserman, 1996; Zwietering, Jongenburger, Rombouts, & Riet, 1990) and Gompertz (Gibson et al., 1987; Gompertz, 1825; Zwietering et al., 1990) equations are widely used in predictive microbiology studies. The original forms of logistic and Gompertz expressions, which are included in Table 1 (Eqs. (1) and (2)), describe a growth tendency (Fig. 1a; a is the asymptotic value of both functions and b and c are shape parameters). These functions were reparameterised by Zwietering et al. (1990), to parameters with biological meaning for microorganisms growth.

Table 1
The logistic and Gompertz models reparameterisation for autocatalytic behaviour

Function	Original ^a	Modified ^b	Reparameterised ^b
Logistic	$y = \frac{a}{1 + \exp(b - cx)}$ (1) x as independent variable	$y = a - \frac{a}{1 + \exp(b - cx)}$ (3) x as independent variable	$\frac{C}{C_0} = \frac{1}{1 + \exp[2k_{\max}(\lambda - t) + 1]}$ (5) t as independent variable
Gompertz	$y = a \exp[-\exp(b - cx)]$ (2) x as independent variable	$y = a - a \exp[-\exp(b - cx)]$ (4) x as independent variable	$\frac{C}{C_0} = 1 - \exp\{-\exp[k_{\max}e(\lambda - t) + 1]\}$ (6) t as independent variable

^a Zwietering et al. (1990).

^b This study.

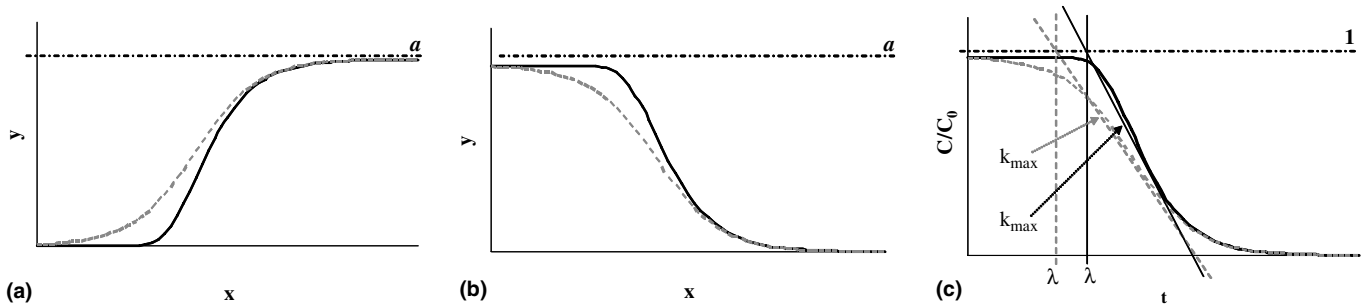


Fig. 1. The mathematical behaviour of the Gompertz (solid black line) and logistic (dashed grey line) equations in the original form (a), modified to describe inactivation behaviour (b) and reparameterised (c).

For the case of inactivation behaviour/degradation kinetics, the expressions can be modified (see also Table 1, Eqs. (3) and (4), Fig. 1b). For an autocatalytic chemical reaction, more convenient reparameterised mathematical forms can represent the variation of the normalized reactant concentration C/C_0 with time (t). The parameter a becomes 1, and a maximum reaction rate, k_{\max} (determined by the slope of the steepest tangent to the exponential phase), and a lag time, λ (calculated by the interception of the asymptote with the extrapolated tangent line), can be used (Table 1, Eqs. (5) and (6), Fig. 1c).

2.2. Modelling temperature and concentration effects on a degradation reaction

Temperature is known to have a significant effect on food reactions kinetics. This effect is often translated into a dependence of the kinetic parameters on temperature, which has been widely studied and can be generally expressed with an Arrhenius type equation using a finite reference temperature (Cohen, Birk, Mannheim, & Saguy, 1994; Haralampu, Saguy, & Karel, 1985; Peleg, 1992; van Boekel, 1996):

$$p = p_{\text{ref}} \exp\left(-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_{\text{ref}}}\right)\right) \quad (7)$$

where p is a kinetic parameter, E_a is activation energy, p_{ref} the kinetic parameter at finite reference temperature, T_{ref} , and R the universal gas constant. Several studies indicated

that if T_{ref} corresponds to the middle temperature of the experimental range, the correlation between parameters and the confidence intervals will be minimised (Brandão, 2004; Cohen et al., 1994; van Boekel, 1996), thus improving the mathematical modelling quality.

Reactant concentration and water content may also affect reactions kinetics. This effect can be included in the Arrhenius parameters (Eq. (7); p_{ref} and E_a), on the basis of experimental data and fitting procedures.

A mixed-model, that includes the influence of one or more main effects and significant interactions, may account empirically for a mathematical description of food reaction kinetics (Saguy & Karel, 1980).

3. Materials and methods

3.1. Preparation of the concentrated sucrose solutions

The selected sucrose concentrations were 70%, 75%, 83%, 87.5% and 97% (w/w).

Sucrose solutions of 70–87.5% (w/w) were prepared by weighing commercial sucrose and adding distilled water in the desired proportion. The mixtures were then heated in a microwave oven (medium power) for short periods (1 min), intercalated with agitation until complete sucrose dissolution (Braga da Cruz, MacInnes, Oliveira, & Malcata, 2002).

To prepare sucrose solutions of 97% (w/w), freeze-dried sucrose (commercial) was equilibrated with a saturated salt

solution of lithium bromide (purum p.a., Fluka), of $a_{w@27^{\circ}\text{C}}$ 6%, under vacuum, until constant weight.

3.2. Water content determination

A Karl Fisher coulometric determination (684 K coulometer, Metrohm, Switzerland) was used to measure the real moisture content of concentrated sucrose solutions. At least three different batches were prepared for each concentration and each batch was analysed three times. The 95% standard error (SE) of the sample water content was calculated.

3.3. Heat treatment of concentrated sucrose solutions

The concentrated sucrose solutions were poured into Thermal Death Time (TDT) cans, 6 cm diameter and 0.8 cm height (208 × 0.06, American National Can, USA), sealed under vacuum, and processed isothermally at 100, 120, 140, 160 and 180 °C in an oil bath (polyethylene glycol 400, Clariant) for different times.

3.4. Analytical determination of sucrose content

After processing, the samples were transferred into a flask and weighed. Water was added and the diluted samples were weighed and frozen for posterior analysis.

Sucrose content of the heat treated solutions was determined using high pressure liquid chromatography. Standard solutions were prepared from sucrose (for biochemistry, Merck). Both samples and standard solutions were injected (AS-15550, Jasco, Japan) in a HPLC system, using a pump (PU-1580, Jasco) with a NH_2 (Merck Licrospher[®]100 NH_2 5 μm) column. The mobile phase, acetonitrile (Isocratic Grade, Lichrosolv, Merck)/water (80:20), was running at 1.5 ml/min. The peaks were detected using a Refractive Index detector (RI-1530, Jasco) and analysed using Jasco–Borwin software v.1.50 (JMBS Developments, Fontaine, France).

3.5. Statistical procedures

3.5.1. Experimental design

Previous analyses were performed in order to evaluate if water content and temperature had a significant effect on sucrose thermal degradation. Experiments were conducted following a 2^2 design (Box, Hunter, & Hunter, 1978) at two water content levels (30.03 and 3.58 (w/w%)) and two temperature levels (120 and 160 °C). Results were analysed using Experimental Design package of STATISTICA[™] v 6.0 (Statsoft[®], Tulsa, OK, USA).

3.5.2. Non-linear regression analysis

The equations mentioned along the text were fitted to data by non-linear regression analysis, using a package of STATISTICA[™] v 6.0. The Levenberg–Marquadt algorithm for the least squares function minimisation was used. The statistical indicators of the quality of the regression,

coefficient of determination (R^2) and the mean square error (MSE, i.e. the sum of squares of residuals divided by the corresponding degrees of freedom), and the 95% standard error of the parameters (SE) were obtained directly from the software. The precision of the estimated parameters was also evaluated by the standardised half width (SHW), which was defined as the ratio between the 95% standard error and the value of the estimate.

4. Results and discussion

4.1. Water content of the concentrated sucrose solutions

The water content of the sucrose solutions is presented in Table 2. Since high temperatures are used in samples preparation, some evaporation occurs, which may explain in some cases lower water content values than expected from the “nominal” concentration, i.e. the concentration calculated with the commercial sucrose and water weights used in the solutions preparation.

4.2. Factorial design analysis

A factorial analysis was previously performed in order to test the influence of water content and temperature on the reaction. These effects, if existent, will be translated into an effect on the kinetic parameters of either of the two models (see Table 1) chosen for the analysis.

Table 2
Water content of the prepared concentrated sucrose solutions (nominal concentration), corresponding standard error (SE) at 95% and sucrose concentration

Nominal sucrose concentration (w/w%)	Water content \pm 95% SE (w/w%)	Sucrose concentration (w/w%)
70.00	30.03 \pm 0.28	69.97
75.00	25.30 \pm 0.63	74.70
83.00	16.32 \pm 0.82	83.68
87.50	12.20 \pm 0.42	87.80
97.00	3.58 \pm 0.50	96.42

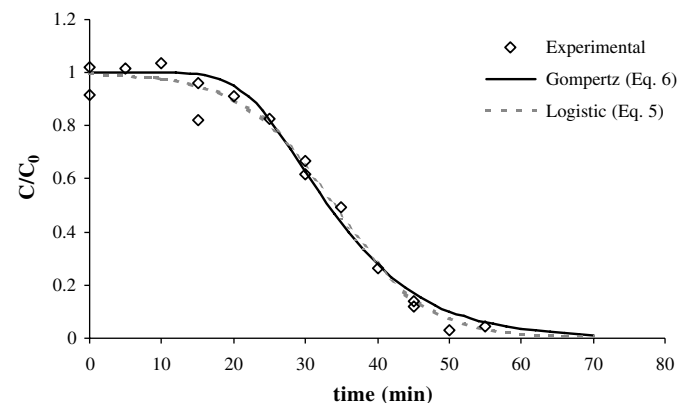


Fig. 2. Results from fitting the logistic (Eq. (5)) and Gompertz (Eq. (6)) models to the experimental data. Example is for a 25.30 (w/w%) water content sucrose solution processed at 140 °C.

The logistic function (Eq. 5) was then fitted to experimental data of sucrose thermal degradation and k_{\max} and λ parameters were estimated.

The analysis of variance (ANOVA) showed that λ and k_{\max} estimates were significantly affected by temperature and water content ($P < 0.05$). Regarding the combined effect, λ was also affected at 5% significance

level, whereas k_{\max} was only significantly affected at an 8% level.

These results clearly demonstrate that sucrose thermal degradation is influenced by temperature and water content of the solutions. In face of that, a study with the objective of modelling these effects on the reaction was conducted, in a wider temperature and water content range.

Table 3

Results from fitting the logistic and Gompertz models to experimental data. Estimates of the parameters, 95% SE and SHW. Indicators of the quality of the regression, R^2 and MSE

Model	W (% w/w)	T (°C)	MSE	R ²	k _{max} (min ⁻¹)	SHW (%)	λ (min)	SHW (%)	
Logistic (Eq. (5))	30.03	100	1.95 × 10 ⁻²	0.881	2.43 × 10 ⁻³ ± 9.88 × 10 ⁻⁴	40.58	431.20 ± 124.94	28.97	
		120	4.30 × 10 ⁻³	0.967	1.29 × 10 ⁻² ± 2.44 × 10 ⁻³	18.90	100.47 ± 10.80	10.75	
		140	7.04 × 10 ⁻³	0.953	7.57 × 10 ⁻² ± 2.15 × 10 ⁻²	28.42	21.89 ± 2.78	12.68	
		160	2.91 × 10 ⁻²	0.776	1.79 × 10 ⁻¹ ± 8.63 × 10 ⁻²	48.35	6.14 ± 1.79	29.13	
	25.30	100	9.65 × 10 ⁻³	0.918	1.73 × 10 ⁻³ ± 5.66 × 10 ⁻⁴	32.68	563.68 ± 127.36	22.59	
		120	1.13 × 10 ⁻²	0.933	1.86 × 10 ⁻² ± 8.75 × 10 ⁻³	47.03	121.70 ± 19.24	15.81	
		140	4.29 × 10 ⁻³	0.973	7.84 × 10 ⁻² ± 1.83 × 10 ⁻²	23.28	27.52 ± 2.20	8.00	
		160	2.57 × 10 ⁻²	0.773	2.41 × 10 ⁻¹ ± 1.13 × 10 ⁻¹	46.91	7.24 ± 1.42	19.63	
	16.32	100	1.72 × 10 ⁻²	0.913	1.51 × 10 ⁻³ ± 8.72 × 10 ⁻⁴	57.89	1343.32 ± 248.31	18.48	
		120	9.09 × 10 ⁻³	0.934	1.39 × 10 ⁻² ± 6.64 × 10 ⁻³	47.88	186.74 ± 23.58	12.63	
		140	1.96 × 10 ⁻²	0.854	5.45 × 10 ⁻² ± 3.31 × 10 ⁻²	60.67	33.01 ± 7.65	23.17	
		160	1.95 × 10 ⁻³	0.988	2.88 × 10 ⁻¹ ± 6.58 × 10 ⁻²	22.82	9.63 ± 0.53	5.46	
	12.20	100	7.92 × 10 ⁻³	0.945	7.70 × 10 ⁻⁴ ± 2.29 × 10 ⁻⁴	29.69	985.29 ± 259.19	26.31	
		120	4.36 × 10 ⁻³	0.972	5.47 × 10 ⁻³ ± 1.33 × 10 ⁻³	24.31	203.64 ± 30.59	15.02	
		140	1.62 × 10 ⁻²	0.844	1.72 × 10 ⁻² ± 6.02 × 10 ⁻³	34.92	35.98 ± 14.50	40.30	
		160	2.05 × 10 ⁻²	0.909	1.67 × 10 ⁻¹ ± 1.21 × 10 ⁻¹	72.59	14.73 ± 3.49	23.70	
		180	3.29 × 10 ⁻²	0.811	2.48 × 10 ⁻¹ ± 1.72 × 10 ⁻¹	69.55	4.12 ± 2.02	48.92	
	3.58	100	5.30 × 10 ⁻²	0.703	2.47 × 10 ⁻⁴ ± 1.02 × 10 ⁻⁴	41.20	3645.19 ± 1164.62	31.95	
		120	7.57 × 10 ⁻³	0.952	2.38 × 10 ⁻³ ± 4.85 × 10 ⁻⁴	20.40	318.73 ± 60.82	19.08	
		140	4.54 × 10 ⁻²	0.807	1.97 × 10 ⁻² ± 1.22 × 10 ⁻²	62.00	101.62 ± 20.91	20.58	
		160	2.54 × 10 ⁻²	0.852	4.65 × 10 ⁻² ± 2.13 × 10 ⁻²	45.76	23.50 ± 7.30	31.08	
		180	2.19 × 10 ⁻²	0.875	2.36 × 10 ⁻¹ ± 1.37 × 10 ⁻¹	57.90	5.10 ± 1.83	35.92	
	Gompertz (Eq. (1))	30.03	100	1.84 × 10 ⁻²	0.888	1.28 × 10 ⁻³ ± 4.91 × 10 ⁻⁴	38.35	218.49 ± 163.86	75.00
			120	4.97 × 10 ⁻³	0.962	6.38 × 10 ⁻³ ± 1.27 × 10 ⁻³	19.95	55.18 ± 16.64	30.16
140			6.81 × 10 ⁻³	0.955	3.80 × 10 ⁻² ± 1.05 × 10 ⁻²	27.70	14.40 ± 3.89	27.03	
160			2.97 × 10 ⁻²	0.771	8.97 × 10 ⁻² ± 4.39 × 10 ⁻²	48.94	3.01 ± 2.60	86.37	
25.30		100	1.47 × 10 ⁻²	0.875	8.26 × 10 ⁻⁴ ± 3.33 × 10 ⁻⁴	40.31	206.88 ± 238.51	115.29	
		120	9.69 × 10 ⁻³	0.943	9.41 × 10 ⁻³ ± 4.10 × 10 ⁻³	43.54	91.68 ± 25.17	27.45	
		140	5.32 × 10 ⁻³	0.966	4.08 × 10 ⁻² ± 1.09 × 10 ⁻²	26.62	20.91 ± 3.52	16.82	
		160	3.07 × 10 ⁻²	0.729	1.55 × 10 ⁻¹ ± 8.57 × 10 ⁻²	55.43	6.05 ± 1.90	31.45	
16.32		100	1.64 × 10 ⁻²	0.917	7.14 × 10 ⁻⁴ ± 3.84 × 10 ⁻⁴	53.79	916.00 ± 369.35	40.32	
		120	7.41 × 10 ⁻³	0.946	6.28 × 10 ⁻³ ± 2.75 × 10 ⁻³	43.85	138.34 ± 34.22	24.73	
		140	2.08 × 10 ⁻²	0.845	2.98 × 10 ⁻² ± 1.87 × 10 ⁻²	62.84	24.47 ± 10.76	43.97	
		160	2.40 × 10 ⁻³	0.985	1.36 × 10 ⁻¹ ± 3.01 × 10 ⁻²	22.23	7.46 ± 0.83	11.08	
12.20		100	6.68 × 10 ⁻³	0.953	3.93 × 10 ⁻⁴ ± 1.03 × 10 ⁻⁴	26.29	274.91 ± 339.90	123.64	
		120	2.23 × 10 ⁻³	0.986	2.69 × 10 ⁻³ ± 4.53 × 10 ⁻⁴	16.80	96.76 ± 31.29	32.34	
		140	1.65 × 10 ⁻²	0.841	8.90 × 10 ⁻³ ± 2.97 × 10 ⁻³	33.41	5.47 ± 19.92	364.14	
		160	1.79 × 10 ⁻²	0.920	8.49 × 10 ⁻² ± 5.49 × 10 ⁻²	64.67	11.27 ± 4.42	39.22	
		180	3.22 × 10 ⁻²	0.815	1.20 × 10 ⁻¹ ± 8.03 × 10 ⁻²	66.76	1.63 ± 2.95	181.55	
3.58		100	4.88 × 10 ⁻²	0.727	1.23 × 10 ⁻⁴ ± 4.62 × 10 ⁻⁵	37.63	1299.80 ± 1540.52	118.52	
		120	6.63 × 10 ⁻³	0.958	1.16 × 10 ⁻³ ± 2.11 × 10 ⁻⁴	18.11	63.45 ± 70.47	111.06	
		140	4.51 × 10 ⁻²	0.808	8.59 × 10 ⁻³ ± 4.97 × 10 ⁻³	57.88	64.61 ± 32.55	50.37	
		160	2.28 × 10 ⁻²	0.868	2.35 × 10 ⁻² ± 9.88E × 10 ⁻³	42.06	10.78 ± 9.69	89.84	
		180	2.02 × 10 ⁻²	0.885	1.15 × 10 ⁻¹ ± 6.04 × 10 ⁻²	52.53	2.56 ± 2.49	97.53	

4.3. Kinetic behaviour of thermal degradation of sucrose in concentrated solutions

A typical behaviour of sucrose thermal degradation data can be observed in Fig. 2 and the results from fitting the logistic and Gompertz equations are presented in Table 3. It can be observed that both models present a similar quality of the regression, assessed by satisfactory R^2 values (varying between 0.703 and 0.988) and identical MSE. However, the precision of λ estimates, evaluated on the basis of SHW, is clearly better for the logistic model in all studied conditions. Moreover, a decrease on the precision of the Gompertz λ parameter is observed as water content decreases. This may be explained by the fact that highly sucrose concentrated samples are more difficult to handle and thus might be subjected to higher experimental errors. Regarding k_{max} precision, considerable differences were not observed, either between the two models or between the high and low water content regimes.

It is interesting to note that the estimates of k_{max} from the logistic function (Eq. (5)) are consistently higher than k_{max} estimates from Gompertz model (Eq. (6)), which may be justified by the different function shapes (Fig. 1). An identical observation was found for the λ parameter. In the logistic function, the lag corresponds to the time necessary to consume 26.9% of the initial sucrose content, while in the Gompertz model it corresponds to 6.6%.

Overall it can be concluded that both models describe the data satisfactorily, as it can be observed by the example in Fig. 2.

4.4. Effect of temperature and water content on the kinetic parameters

In order to ascertain the temperature effect on the reaction kinetics an Arrhenius type dependence of k_{max} and λ (in Eq. (7) the p parameter becomes k_{max} or λ) was assumed. The final logistic and Gompertz models thus obtained (Eqs. (8) and (9)):

$$\frac{C}{C_0} = \frac{1}{1 + \exp \left\{ 2k_{max,ref} \exp \left[\frac{-E_{ak_{max}}}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) \right] \left[\lambda_{ref} \exp \left[\frac{E_{a\lambda}}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) \right] - t \right] + 1 \right\}} \tag{8}$$

$$\frac{C}{C_0} = 1 - \exp \left\{ - \exp \left[ek_{max,ref} \exp \left[\frac{-E_{ak_{max}}}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) \right] \right] \times \left[\lambda_{ref} \exp \left[\frac{E_{a\lambda}}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) \right] - t \right] + 1 \right\} \tag{9}$$

were fitted to the experimental data at all temperatures (Arabshahi & Lund, 1985; Cohen & Saguy, 1985; Haralampu et al., 1985; Lund, 1983), at constant water content.

Results of the regressions can be seen in Table 4. The indicators of the quality of the regression, R^2 and MSE, indicated a good regression procedure in all cases. Estimates precision is similar in both models. The behaviour of k_{max} and λ , as a function of temperature, can also be observed in Fig. 3.

Table 4 Results of Arrhenius equation fitting to k_{max} and λ parameters, obtained using the logistic (Eq. (5)) and Gompertz (Eq. (6)) equations

Model	Water (% w/w)	MSE	R^2	k_{max}		λ		$E_{ak_{max}}$ (kJ mol ⁻¹)	SHW (%)	$E_{a\lambda}$ (kJ mol ⁻¹)	SHW (%)
				$k_{max,ref}$ (min ⁻¹)	SHW (%)	λ_{ref} (min)	SHW (%)				
Logistic	30.03	1.64×10^{-2}	0.886	$5.61 \times 10^{-2} \pm 1.13 \times 10^{-2}$	20.07	98.67 ± 10.77	10.91	22.15 ± 2.46	11.12	96.28 ± 6.40	6.65
	25.30	1.46×10^{-2}	0.888	$6.98 \times 10^{-2} \pm 1.44 \times 10^{-2}$	20.62	113.52 ± 11.14	9.82	27.77 ± 2.17	7.81	95.91 ± 5.15	5.37
	16.32	1.65×10^{-2}	0.890	$5.74 \times 10^{-2} \pm 1.76 \times 10^{-2}$	30.66	115.66 ± 15.92	13.76	37.88 ± 3.50	9.24	110.58 ± 5.25	4.74
	12.20	1.74×10^{-2}	0.876	$2.18 \times 10^{-2} \pm 4.21 \times 10^{-3}$	19.30	105.29 ± 10.07	9.56	46.48 ± 6.26	13.48	94.64 ± 7.24	7.65
	3.58	3.84×10^{-2}	0.788	$1.23 \times 10^{-2} \pm 3.03 \times 10^{-3}$	24.63	121.55 ± 11.38	9.36	94.12 ± 13.41	14.25	111.81 ± 7.30	6.53
Gompertz	30.03	1.52×10^{-2}	0.889	$2.85 \times 10^{-2} \pm 5.63 \times 10^{-3}$	19.80	98.47 ± 10.38	10.54	12.33 ± 3.44	27.91	94.21 ± 16.10	17.09
	25.30	1.50×10^{-2}	0.877	$3.89 \times 10^{-2} \pm 8.70 \times 10^{-3}$	22.39	118.39 ± 9.94	8.40	20.48 ± 3.26	15.90	84.01 ± 10.58	12.60
	16.32	1.38×10^{-2}	0.899	$3.09 \times 10^{-2} \pm 8.70 \times 10^{-3}$	28.12	125.82 ± 12.51	9.94	28.80 ± 4.37	15.17	100.55 ± 9.51	9.46
	12.20	1.53×10^{-2}	0.885	$1.09 \times 10^{-2} \pm 1.97 \times 10^{-3}$	18.08	106.61 ± 7.46	7.00	18.69 ± 9.34	49.98	75.99 ± 21.23	27.93
	3.58	3.43×10^{-2}	0.805	$6.08 \times 10^{-3} \pm 1.40 \times 10^{-3}$	23.07	124.69 ± 8.64	6.93	42.44 ± 18.78	44.26	93.34 ± 19.50	20.89

Note: T_{ref} is the calculated middle temperature of the experimental range: 140 °C.

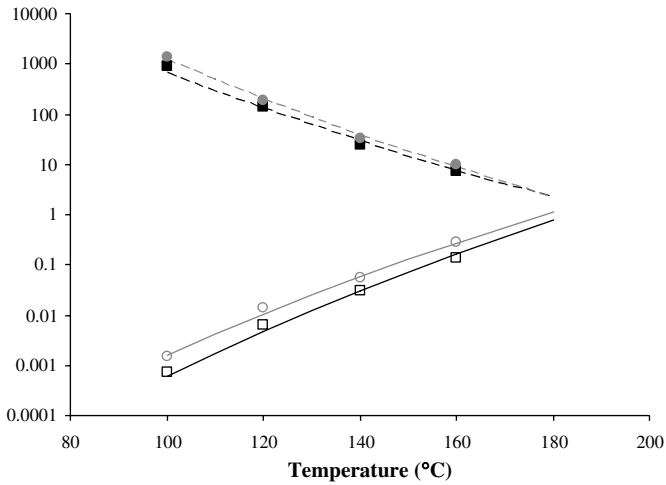


Fig. 3. Comparison of k_{\max} (open symbols) and λ (filled symbols) estimated using: (i) the logistic function (Eq. (5)) (grey circles) and (ii) the Gompertz model (Eq. (6)) (black squares) with Arrhenius one-step prediction of k_{\max} (solid lines) and λ (dashed lines) using Eqs. (8) (grey lines) and (9) (black lines). Example corresponds to experimental results using 16.32 (w/w%) water content sucrose solution.

In order to study the water content effect on the reaction, as a first approach, the estimated kinetic parameters (Table 4) were plotted against concentration (Fig. 4). No significant water content effect was observed for the activation energy, for both k_{\max} and λ (Fig. 4b and d). A similar result was observed for inactivation kinetics of freeze dried α -amylase (Saraiva, Oliveira, Hendrickx, Oliveira, &

Tobback, 1996). However, several other works found a moisture content (or water activity) effect on E_a . Nevertheless, most of those studies do not refer the precision of the estimates (e.g. confidence intervals) (Erenturk, Gulaboglu, & Gultekin, 2005; Kaymak-Ertekin & Gedik, 2005; Labuza, 1980; Pedreschi, Moyano, Kaack, & Granby, 2005) and consequently, inference about their significance is impaired. When the precision of the estimates was presented and the water activity effect on E_a was significant, it was only meaningful in extreme limits of an overall range (Manan, Baines, Stone, & Ryley, 1995; Rapusas & Driscoll, 1995). The pre-exponential factor of k_{\max} , $k_{\max,ref}$ (Eqs. (8) and (9)), varies linearly with water content (Fig. 4a). Concerning λ_{ref} , water content has a linear effect on the Gompertz parameter and an exponential relation was found for the logistic one. These effects can be summarised as:

$$E_{ak_{\max}(\text{logistic or Gompertz})} = C_1 \tag{10}$$

$$E_{a\lambda(\text{logistic or Gompertz})} = C_2 \tag{11}$$

$$k_{\max,ref(\text{logistic or Gompertz})} = C_3 W \tag{12}$$

$$\lambda_{ref(\text{logistic})} = C_4 \exp(C_5 W) \tag{13}$$

$$\lambda_{ref(\text{Gompertz})} = C_6 + C_7 W \tag{14}$$

where C_1 to C_7 are constants and W represents the water content (%(w/w)).

These relations (Eqs. (10)–(14)) were embedded in the two models (Eqs. (8) and (9)) to globally describe the

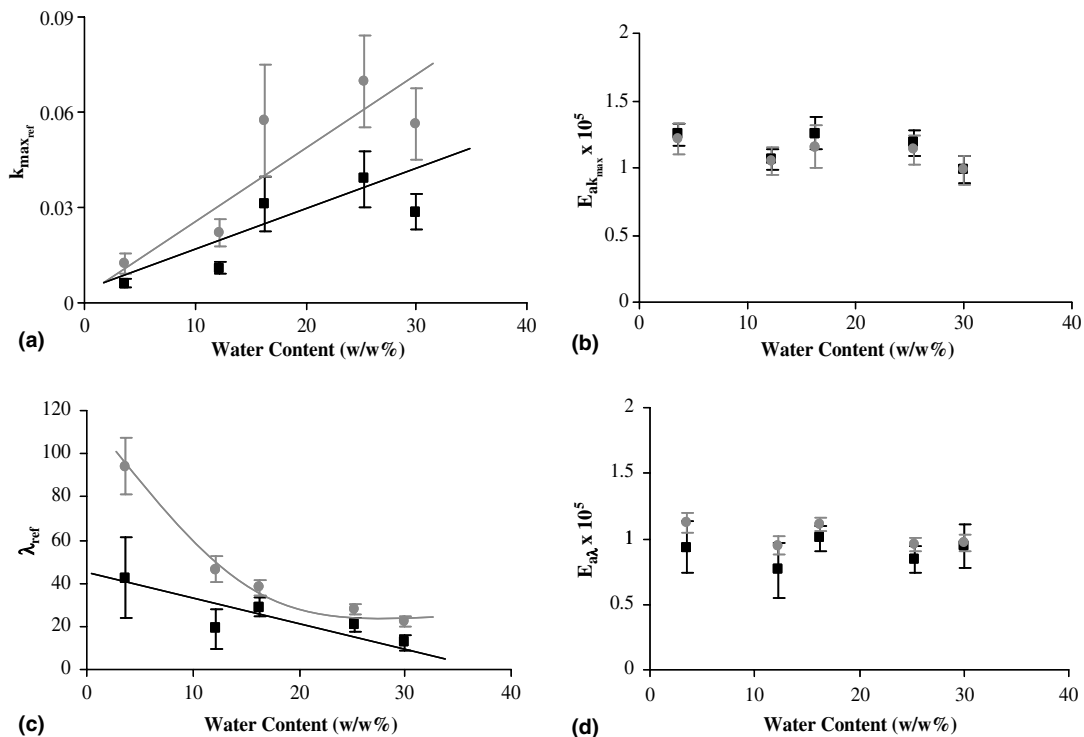


Fig. 4. Effect of concentration on the parameters from logistic (Eq. (8), grey circles) and Gompertz (Eq. (9), black squares) equations. The bars indicate the 95% confidence limit of each parameter.

Table 5

Results of global logistic and Gompertz models fitting to experimental data. Evaluation of the quality of the regression on the basis of MSE, R^2 and residuals randomness and normality. Estimates precision is evaluated using the 95% SE and SHW%

	Global logistic		Global Gompertz	
		SHW (%)		SHW (%)
$E_{ak_{max}} (C_1)$	$1.16 \times 10^5 \pm 5.60 \times 10^3$	4.8	$1.19 \times 10^5 \pm 4.05 \times 10^3$	3.4
$E_{a\lambda} (C_2)$	$9.98 \times 10^4 \pm 3.39 \times 10^3$	3.4	$8.40 \times 10^4 \pm 6.21 \times 10^3$	7.4
C_3	$2.55 \times 10^{-3} \pm 2.96 \times 10^{-4}$	11.6	$1.39 \times 10^{-3} \pm 1.37 \times 10^{-4}$	9.8
C_4	$9.28 \times 10^1 \pm 1.12 \times 10^1$	12.1		
C_5	$-4.88 \times 10^{-2} \pm 5.27 \times 10^{-3}$	10.8		
C_6			$3.51 \times 10^1 \pm 6.50 \times 10^0$	18.5
C_7			$-6.31 \times 10^{-1} \pm 2.17 \times 10^{-1}$	34.4
R^2		0.808	0.830	
MSE	2.95×10^{-2}		2.62×10^{-2}	
<i>Residuals</i>				
Normality	+		+	
Randomness	+		+	

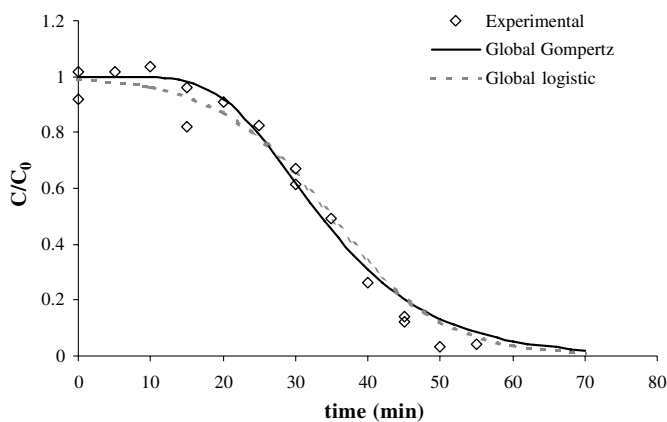


Fig. 5. Global fit of logistic and Gompertz models to the experimental data. Example is for a 25.30 (w/w%) water content solution processed at 140 °C.

temperature and water content dependence of sucrose thermal degradation.

The results from global fit of logistic and Gompertz models to experimental data are presented in Table 5. Once again it was assessed the adequacy of both models (Fig. 5) and the parameters were estimated with acceptable precision.

Furthermore, the observed concentration and temperature dependence of k_{max} and λ kinetic parameters reinforces the idea of the importance of molecular mobility in sucrose thermal degradation reaction. It was also observed a decrease in solutions pH (results not shown) along processing time, which could also be responsible for the autocatalytic behaviour of the reaction.

5. Conclusions

Results of isothermal kinetic experiments conducted on concentrated neutral solutions of pure sucrose, at temperatures ranging from 100 to 180 °C and using solutions with varying water content (3.58–30.03 (% w/w)), showed a lag phase, which was previously described in literature. The

logistic and Gompertz equations were modified and reparameterised in order to describe reactions behaviour with kinetic parameters with physical meaning (k_{max} and λ). These models were able to successfully describe reaction's autocatalytic behaviour. The lag phase and reactions rate, described by λ and k_{max} , respectively, were dependent on both temperature and water content. The parameters dependence on temperature was described by Arrhenius type equations. The water content dependence was observed on the Arrhenius parameters. Global logistic and Gompertz models were proposed, which were able to successfully describe experimental data in the studied temperature and concentration intervals. These observations reinforce the idea of the importance of molecular mobility in sucrose thermal degradation reaction.

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